



## Low-activation concrete design of the Danish Center for Particle Therapy

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# Low-activation concrete design of the Danish Center for Particle Therapy

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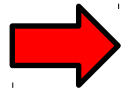
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# Motivation









- Neutrons induce **significant radioactivity** in the concrete walls close to the energy degrader
- If activity concentration  $>$  EU exemption level at the end-of-life of DCPT



**Significant cost** for wall demolition, transport, and long-term storage of radioactive concrete



## Radiation safety design of proton centers:

Design tasks	Traditional	DCPT
Shielding barrier thickness		
MC modeling of concrete activation		
Development of a dedicated low-activation concrete		
Full low-activation bunker design for walls, floor, and ceiling		

Trento: MC simulation in forward direction + special sand with low Eu content

Uppsala: Marble concrete walls in the cyclotron and ESS bunker

# Long-lived radionuclides in concrete

Most common neutron-induced long-lived radionuclides in concrete:

Radio-nuclide	Dominant production mechanism	Half life (years)	EU exemption level (kBq/kg)
Cs-134	$^{133}\text{Cs}(n,\gamma)$	2.06 y	0.1
Na-22	$^{23}\text{Na}(n,2n)$ , $^{27}\text{Al}(n,\alpha+2n)$ , $^{24}\text{Mg}(n,p+2n)$ , $^{28}\text{Si}(n,n+2p+\alpha)$	2.60	0.1
Co-60	$^{59}\text{Co}(n,\gamma)$	5.27	0.1
H-3	$^6\text{Li}(n,\alpha)$ , $^7\text{Li}(n,\alpha+n)$	12.3	100 (only beta decay)
Eu-152	$^{151}\text{Eu}(n,\gamma)$	13.5	0.1

**Activity > Exemption level:** Material is classified as radioactive waste

# Calculation of concrete activation

Activity of radionuclides in concrete close to DCPT degrader after 30 years of operation of DCPT [1]:

$$a_{radio} = R_{p,1 \text{ year}} \frac{\rho_A}{\rho} \int_0^{250 \text{ MeV}} \Phi(E) \sigma(E) dE \cdot (1 - e^{-\lambda \cdot 30 \text{ years}})$$

$R_{p,1 \text{ year}}$ : Average rate of proton loss

$\Phi(E)$ : Differential neutron fluence per proton

$\sigma(E)$ : Reaction cross section

$\rho_A$ : Atomic density of target nuclides

$\rho$ : Density

$\lambda$ : Decay constant of the radionuclide

## Main input to the calculation:

- $R_{p,1 \text{ year}}$ : Proton workload at the degrader
- $\rho_A$ : Concrete composition
- $\Phi(E)$ : MCNPX MC simulation of neutron fluence
- $\sigma(E)$ : ENDF database , IAEA

1. Shielding Design and Radiation Safety of Charged Particle Therapy Facilities, PTCOG Report 1

# Concrete composition of DCPT concrete

Element	Content (weight %)
C	7.6 %
O	51.1 %
Na	0.8 %
Mg	0.1 %
Al	2.4 %
Si	21.8 %
Ca	13.4 %
Fe	1.5 %
Li	8.6 ppm
Cs	0.46 ppm
Co	3.4 ppm
Eu	0.39 ppm

## DCPT concrete specification:

- Standard concrete with Danish sand and stone
- Density: 2.25 g/cm<sup>3</sup>

Production of Na-22

Production of H-3 and Cs-134

Production of Co-60 and Eu-152

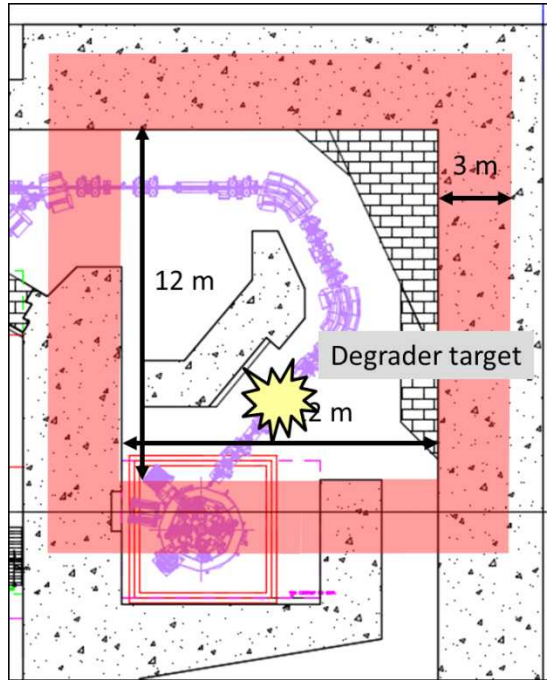
**Steel reinforcement:** 120 ppm cobalt



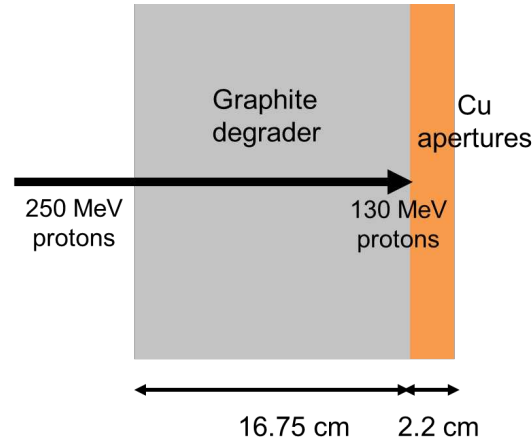
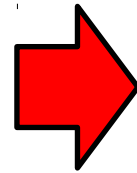
# MC model of ESS bunker

Most protons are lost at the degrader and the nearby Cu apertures

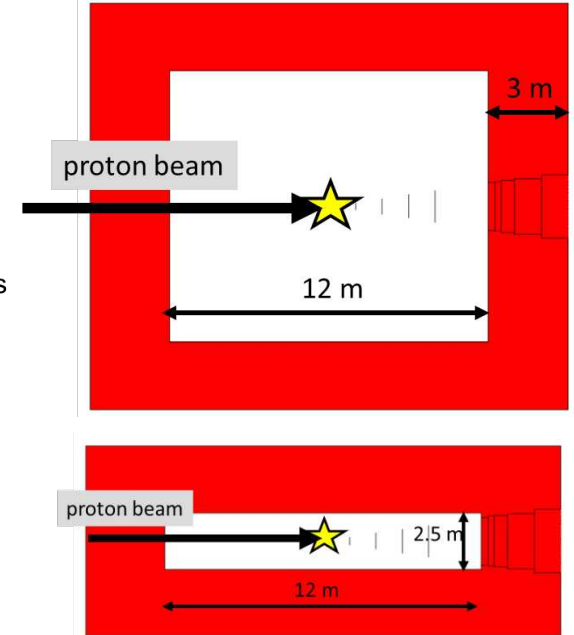
➔ Sufficient with **MC simulation of the ESS bunker**



## MC model of degrader target:



## MC model of ESS bunker walls:





# Activity concentration in ESS bunker walls after 30 years

Radionuclide			Eu-152	Co-60	Co-60	Na-22	Na-22	Na-22	Na-22	Na-22
Material			Concrete	Concrete	Steel rebar	Concrete	Concrete	Concrete	Concrete	Concrete
Target isotope			Eu-151	Co-59	Co-59	Na-23	Al-27	Mg-24	Si-28	Sum
Location	Distance (m)	Depth (m)	Activity concentration (kBq/kg)							
Forward	6	0	0.30	0.08	2.66	0.21	0.09	0.02	0.77	1.09
Forward	6	0.25	0.29	0.07	2.59	0.15	0.06	0.02	0.52	0.75
Floor/ceiling	1.25	0	0.38	0.10	3.43	0.67	0.09	0.02	0.34	1.13
Floor/ceiling	1.25	0.25	0.70	0.17	6.16	0.20	0.03	0.01	0.13	0.37
Side wall:	6	0	0.23	0.06	2.03	0.04	0.00	0.00	0.02	0.06
Exemption level (kBq/kg)			0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1







**Too high activity** of Eu-152, Co-60, and Na-22 for a **large volume of concrete**



**Low-activation concrete** needed close to the degrader

# Low-activation marble concrete

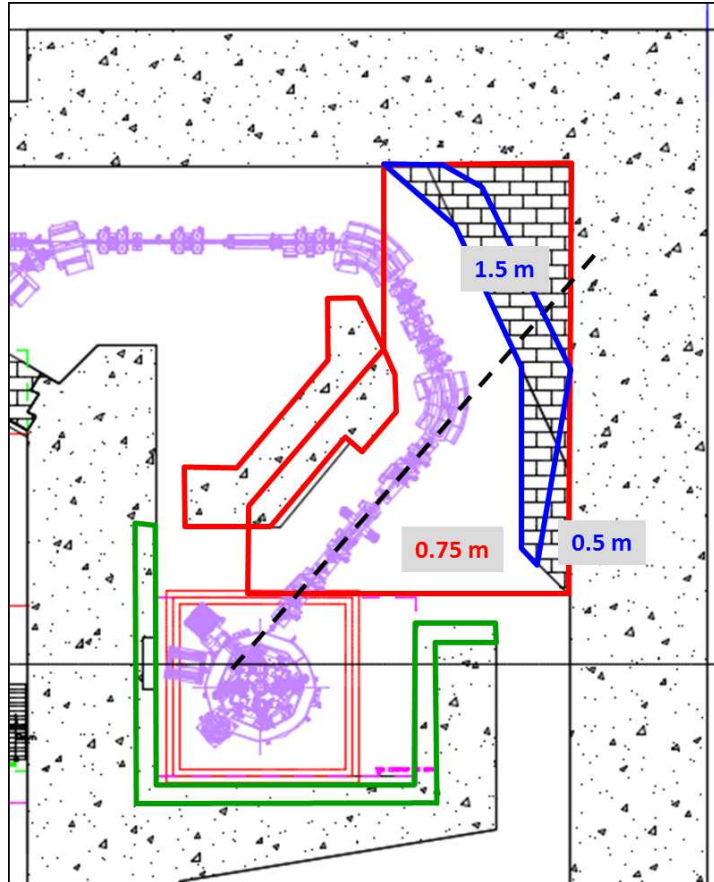
**Marble concrete:** DCPT concrete with sand/stone aggregates replaced by white Norwegian marble

Element	Content (weight %)	Max. allowed content (weight %) without violating exemption level
C	10.4 %	
O	37.4 % 	
Na	<0.2 % 	<b>0.12 %</b>
Mg	0.2 % 	0.43 %
Al	0.6 % 	2.6 %
Si	2.3 %	<b>2.8 %</b>
Ca	47.3 %	
Fe	0.9 %	
Li	3.7 ppm 	128 ppm
Cs	<0.2 ppm 	3.1 ppm
Co	1.8 ppm	<b>1.95 ppm</b>
Eu	<0.1 ppm	<b>0.06 ppm</b>

**White Norwegian marble:**



# Low-activation concrete design of the ESS bunker



## Red area:

- Casting of marble concrete
- Reduce steel reinforcement to a minimum for the first 1 m

Blue area: Blocks of marble concrete

Green area: Avoid steel reinforcement for the first 0.5 m if possible

## After 30 years of DCPT operation:

- Activity conc. in concrete < EU exemption level
- Activity conc. in steel rebar > EU exemption level (limited amount + can easily be separated)

## We have...

- Developed a **general method** for calculation of concrete activation
- Calculated of max. **content of elements in ESS bunker** which do not violate exemption level
- Developed a **new low-activation concrete**
- Designed a **full low-activation bunker (walls, floor, and ceiling)**
  - Low-activity concrete
  - Reduced use of steel reinforcement